

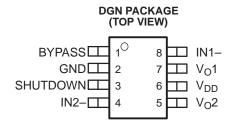


Check for Samples: TPA6110A2

#### **FEATURES**

- 150 mW Stereo Output
- PC Power Supply Compatible
  - Fully Specified for 3.3 V and 5 V Operation
  - Operation to 2.5 V
- Pop Reduction Circuitry
- Internal Mid-Rail Generation
- · Thermal and Short-Circuit Protection

- Surface-Mount Packaging
  - PowerPAD™ MSOP
- Pin Compatible With LM4881

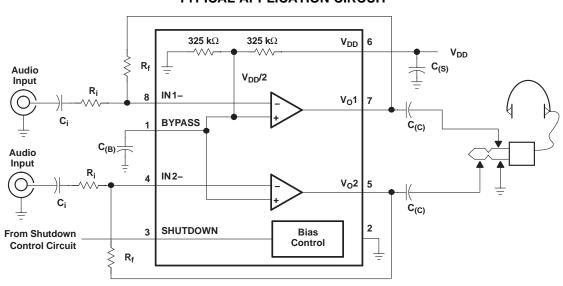


#### **DESCRIPTION**

The TPA6110A2 is a stereo audio power amplifier packaged in an 8-pin PowerPAD™ MSOP package capable of delivering 150 mW of continuous RMS power per channel into 16-Ω loads. Amplifier gain is externally configured by means of two resistors per input channel and does not require external compensation for settings of 1 to 10.

THD+N when driving a 16- $\Omega$  load from 5 V is 0.03% at 1 kHz, and less than 1% across the audio band of 20 Hz to 20 kHz. For 32- $\Omega$  loads, the THD+N is reduced to less than 0.02% at 1 kHz, and is less than 1% across the audio band of 20 Hz to 20 kHz. For 10-k $\Omega$  loads, the THD+N performance is 0.005% at 1 kHz, and less than 0.5% across the audio band of 20 Hz to 20 kHz.

#### TYPICAL APPLICATION CIRCUIT



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These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

#### **AVAILABLE OPTIONS**

т	PACKAGED DEVICE	MSOP SYMBOLIZATION
I A	MSOP <sup>(1)</sup>	MSOP STMBOLIZATION
-40°C to 85°C	TPA6110A2DGN	TI AIZ

(1) The DGN package is available in left-ended tape and reel only (e.g., TPA6110A2DGNR).

#### **PinFunctions**

PIN		1/0	DESCRIPTION	
NAME	NO.	1/0	DESCRIPTION	
BYPASS	1	I	Tap to voltage divider for internal mid-supply bias supply. Connect to a 0.1 $\mu$ F to 1 $\mu$ F low ESR capacitor for best performance.	
GND	2	- 1	GND is the ground connection.	
IN1-	8	I	IN1– is the inverting input for channel 1.	
IN2-	4	I	IN2– is the inverting input for channel 2.	
SHUTDOWN	3	- 1	Puts the device in a low quiescent current mode when held high.	
$V_{DD}$	6	- 1	V <sub>DD</sub> is the supply voltage terminal.	
V <sub>O</sub> 1	7	0	V <sub>O</sub> 1 is the audio output for channel 1.	
V <sub>O</sub> 2	5	0	V <sub>O</sub> 2 is the audio output for channel 2.	

#### ABSOLUTE MAXIMUM RATINGS(1)

over operating free-air temperature range (unless otherwise noted)

		UNIT
$V_{DD}$	Supply voltage	6 V
$V_{I}$	Input voltage	–0.3 V to V <sub>DD</sub> + 0.3 V
	Continuous total power dissipation	Internally limited
T <sub>J</sub>	Operating junction temperature range	-40°C to 150°C
T <sub>stg</sub>	Storage temperature range	-65°C to 150°C

<sup>(1)</sup> Stresses beyond those listed under "absolute maximum ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under "recommended operating conditions" is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

#### **DISSIPATION RATING TABLE**

PACKAGE	T <sub>A</sub> ≤ 25°C	DERATING FACTOR	T <sub>A</sub> = 70°C	T <sub>A</sub> = 85°C
	POWER RATING	ABOVE T <sub>A</sub> = 25°C	POWER RATING	POWER RATING
DGN	2.14 W <sup>(1)</sup>	17.1 mW/°C	1.37 W	1.11 W

<sup>(1)</sup> See the Texas Instruments document, PowerPAD Thermally Enhanced Package Application Report (SLMA002), for more information on the PowerPAD™ package. The thermal data was measured on a PCB layout based on the information in the section entitled Texas Instruments Recommended Board for PowerPAD on page 33 of the before mentioned document.

#### RECOMMENDED OPERATING CONDITIONS

	MINIERDED OF ERVATING CONDITIONS			
		MIN	MAX	UNIT
$V_{DD}$	Supply voltage	2.5	5.5	V
$T_A$	Operating free-air temperature	-40	85	°C
$V_{IH}$	High-level input voltage (SHUTDOWN)	60% x V <sub>DD</sub>		V
$V_{IL}$	Low-level input voltage (SHUTDOWN)		25% x V <sub>DD</sub>	V

Product Folder Link(s): TPA6110A2



#### DC ELECTRICAL CHARACTERISTICS

at  $T_A = 25$ °C,  $V_{DD} = 2.5$  V (unless otherwise noted)

	PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
Voo	Output offset voltage	$A_V = 2 \text{ V/V}$			15	mV
PSRR	Power supply rejection ratio	V <sub>DD</sub> = 3.2 V to 3.4 V		83		dB
I <sub>DD</sub>	Supply current	SHUTDOWN = 0 V		1.5	3	mA
I <sub>DD(SD)</sub>	Supply current in shutdown mode	SHUTDOWN = V <sub>DD</sub>		1	10	μΑ

#### **AC OPERATING CHARACTERISTICS**

 $V_{DD} = 3.3 \text{ V}, T_A = 25^{\circ}\text{C}, R_L = 16 \Omega$ 

	PARAMETER	TEST CONDITIONS	MIN TYP MAX	UNIT
Po	Output power (each channel)	THD≤ 0.1%, f = 1 kHz	60	mW
THD+N	Total harmonic distortion + noise	P <sub>O</sub> = 40 mW, 20 - 20 kHz	0.4%	
B <sub>OM</sub>	Maximum output power BW	G = 10, THD < 5%	> 20	kHz
	Phase margin	Open loop	96°	
	Supply ripple rejection ratio	f = 1 kHz	71	dB
	Channel/channel output separation	f = 1 kHz, P <sub>O</sub> = 40 mW	89	dB
SNR	Signal-to-noise ratio	P <sub>O</sub> = 50 mW, A <sub>V</sub> = 1	100	dB
V <sub>n</sub>	Noise output voltage	A <sub>V</sub> = 1	11	μV(rms)

#### DC ELECTRICAL CHARACTERISTICS

at  $T_A = 25^{\circ}C$ ,  $V_{DD} = 5.5 \text{ V}$  (unless otherwise noted)

αι · <sub>A</sub> – 2	t TA = 20 G, VDD = 6.6 V (arriced currentwice flower)							
	PARAMETER	TEST CONDITIONS	MIN TYP	MAX	UNIT			
Voo	Output offset voltage	A <sub>V</sub> = 2 V/V		15	mV			
PSRR	Power supply rejection ratio	V <sub>DD</sub> = 4.9 V to 5.1 V	76		dB			
I <sub>DD</sub>	Supply current	SHUTDOWN = 0 V	1.5	3	mA			
I <sub>DD(SD)</sub>	Supply current in shutdown mode	SHUTDOWN = V <sub>DD</sub>	1	10	μΑ			
I <sub>IH</sub>	High-level input current (SHUTDOWN)	$V_{DD} = 5.5 \text{ V}, V_I = V_{DD}$		1	μΑ			
I <sub>IL</sub>	Low-level input current (SHUTDOWN)	V <sub>DD</sub> = 5.5 V, V <sub>I</sub> = 0 V		1	μΑ			
Zi	Input impedance		>1		МΩ			

#### **AC OPERATING CHARACTERISTICS**

 $V_{DD} = 5 \text{ V. } T_{\Lambda} = 25^{\circ}\text{C. } R_{L} = 16 \Omega$ 

V <sub>DD</sub> = 0 V, I <sub>A</sub> = 20 G, I <sub>C</sub> = 10 12						
	PARAMETER	TEST CONDITIONS	MIN TYP MAX	UNIT		
Po	Output power (each channel)	THD≤ 0.1%, f = 1 kHz	150	mW		
THD+N	Total harmonic distortion + noise	P <sub>O</sub> = 100 mW, 20 - 20 kHz	0.6%			
B <sub>OM</sub>	Maximum output power BW	G = 10, THD < 5%	> 20	kHz		
	Phase margin	Open loop	96°			
	Supply ripple rejection ratio	f = 1 kHz	61	dB		
	Channel/Channel output separation	f = 1 kHz, P <sub>O</sub> = 100 mW	90	dB		
SNR	Signal-to-noise ratio	P <sub>O</sub> = 100 mW, A <sub>V</sub> = 1	100	dB		
V <sub>n</sub>	Noise output voltage	A <sub>V</sub> = 1	11.7	μV(rms)		

#### **AC OPERATING CHARACTERISTICS**

 $V_{DD} = 3.3 \text{ V}, T_A = 25^{\circ}\text{C}, R_L = 32 \Omega$ 

PARAME	TER	TEST CONDITIONS	MIN TYP MAX	UNIT
Po	Output power (each channel)	THD≤ 0.1%, f = 1 kHz	40	mW
THD+N	Total harmonic distortion + noise	P <sub>O</sub> = 30 mW, 20 - 20 kHz	0.4%	
B <sub>OM</sub>	Maximum output power BW	A <sub>V</sub> = 10, THD < 2%	> 20	kHz

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### **AC OPERATING CHARACTERISTICS (continued)**

 $V_{DD}=3.3~V,~T_A=25^{\circ}C,~R_L=32~\Omega$ 

PARAM	IETER	TEST CONDITIONS	MIN TYP	MAX UN	NIT
	Phase margin	Open loop	96°		
	Supply ripple rejection ratio	f = 1 kHz	71	d	ΙB
	Channel/channel output separation	f = 1 kHz	95	d	ΙB
SNR	Signal-to-noise ratio	$P_{O} = 40 \text{ mW}, A_{V} = 1$	100	d	ΙB
V <sub>n</sub>	Noise output voltage	A <sub>V</sub> = 1	11	μV(ı	rms)

#### **AC OPERATING CHARACTERISTICS**

 $V_{DD}$  = 5 V,  $T_A$  = 25°C,  $R_L$  = 32  $\Omega$ 

PARAME	TER	TEST CONDITIONS	MIN TYP MAX	UNIT
Po	Output power (each channel)	THD≤ 0.1%, f = 1 kHz	90	mW
THD+N	Total harmonic distortion + noise	$P_0 = 60 \text{ mW}, 20 - 20 \text{ kHz}$	0.4%	
B <sub>OM</sub>	Maximum output power BW	A <sub>V</sub> = 10, THD < 2%	> 20	kHz
	Phase margin	Open loop	97°	
	Supply ripple rejection ratio	f = 1 kHz	61	dB
	Channel/channel output separation	f = 1 kHz	98	dB
SNR	Signal-to-noise ratio	$P_{O} = 90 \text{ mW}, A_{V} = 1$	100	dB
V <sub>n</sub>	Noise output voltage	A <sub>V</sub> = 1	11.7	μV(rms)

#### **TYPICAL CHARACTERISTICS**

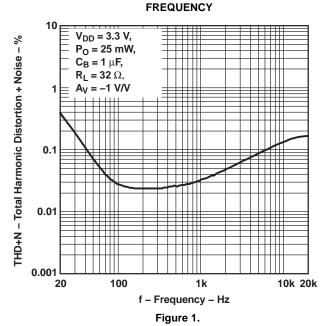
#### **Table of Graphs**

			FIGURE
THD+N	Total harmonia distantian plus poiss	vs Frequency	1, 3, 5, 6, 7, 9, 11, 13
I HD+N	Total harmonic distortion plus noise	vs Output power	2, 4, 8, 10, 12, 14
	Supply ripple rejection ratio	vs Frequency	15, 16
V <sub>n</sub>	Output noise voltage	vs Frequency	17, 18
	Crosstalk	vs Frequency	19–24
	Shutdown attenuation	vs Frequency	25, 26
	Open-loop gain and phase margin	vs Frequency	27, 28
	Output power	vs Load resistance	29, 30
I <sub>DD</sub>	Supply current	vs Supply voltage	31
SNR	Signal-to-noise ratio	vs Voltage gain	32
	Power dissipation/amplifier	vs Load power	33, 34

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# TOTAL HARMONIC DISTORTION + NOISE vs



# TOTAL HARMONIC DISTORTION + NOISE vs OUTPUT POWER

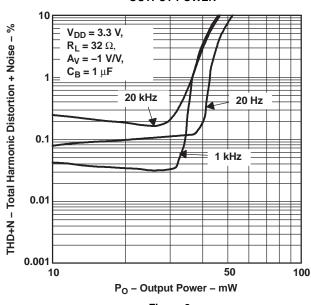
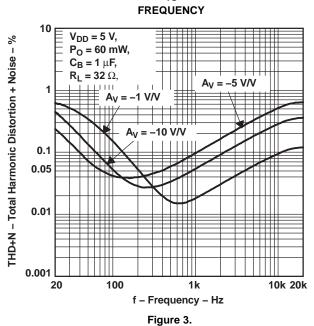


Figure 2.

# TOTAL HARMONIC DISTORTION + NOISE



TOTAL HARMONIC DISTORTION + NOISE

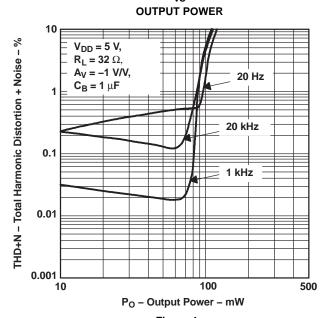
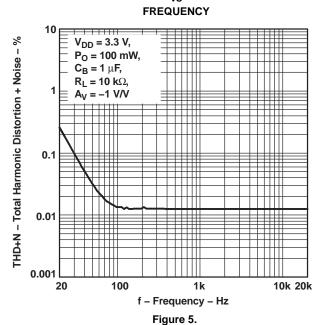


Figure 4.



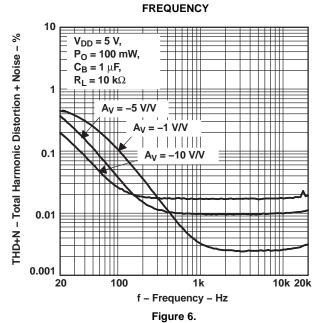
# TOTAL HARMONIC DISTORTION + NOISE



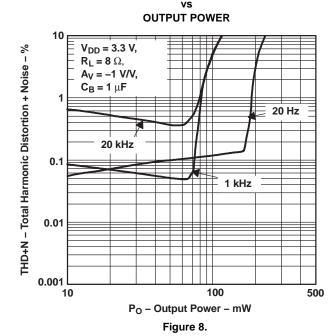
# TOTAL HARMONIC DISTORTION + NOISE vs

## **FREQUENCY** 10 ----THD+N - Total Harmonic Distortion + Noise - % $V_{DD} = 3.3 V,$ $P_0 = 60 \text{ mW},$ $C_B = 1 \mu F$ , $R_L = 8 \Omega$ = -1 V/V0.1 0.01 0.001 20 100 1k 10k 20k f - Frequency - Hz Figure 7.

# TOTAL HARMONIC DISTORTION + NOISE vs

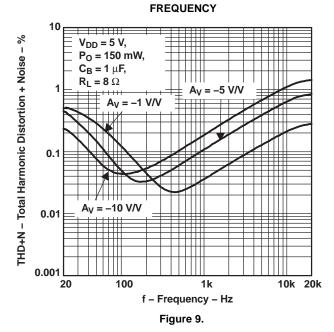


### TOTAL HARMONIC DISTORTION + NOISE

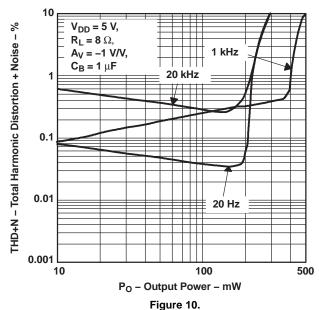




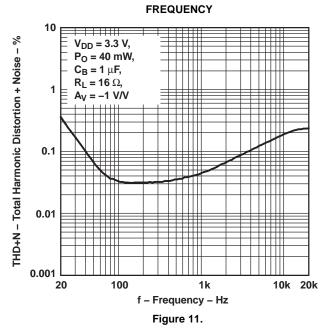
# TOTAL HARMONIC DISTORTION + NOISE vs



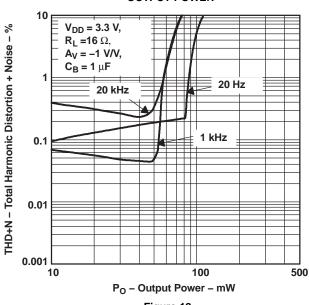
# TOTAL HARMONIC DISTORTION + NOISE vs OUTPUT POWER



# TOTAL HARMONIC DISTORTION + NOISE vs



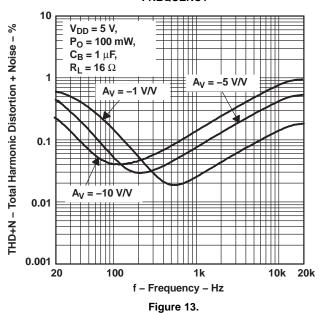
# TOTAL HARMONIC DISTORTION + NOISE vs OUTPUT POWER



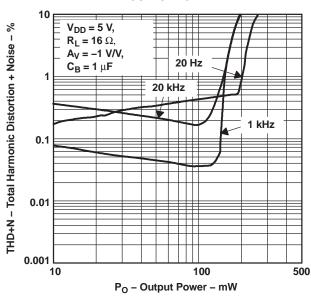


# TOTAL HARMONIC DISTORTION + NOISE

## FREQUENCY

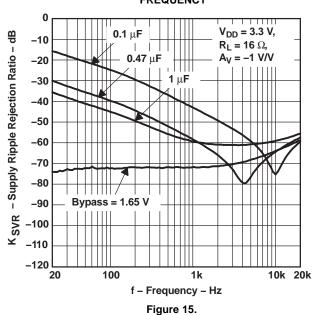


# TOTAL HARMONIC DISTORTION + NOISE vs OUTPUT POWER



#### **SUPPLY RIPPLE REJECTION RATIO**

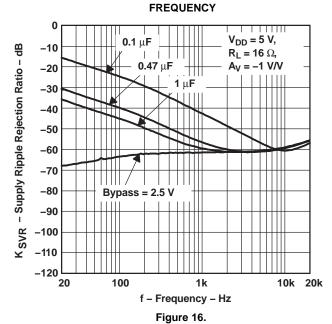
## FREQUENCY



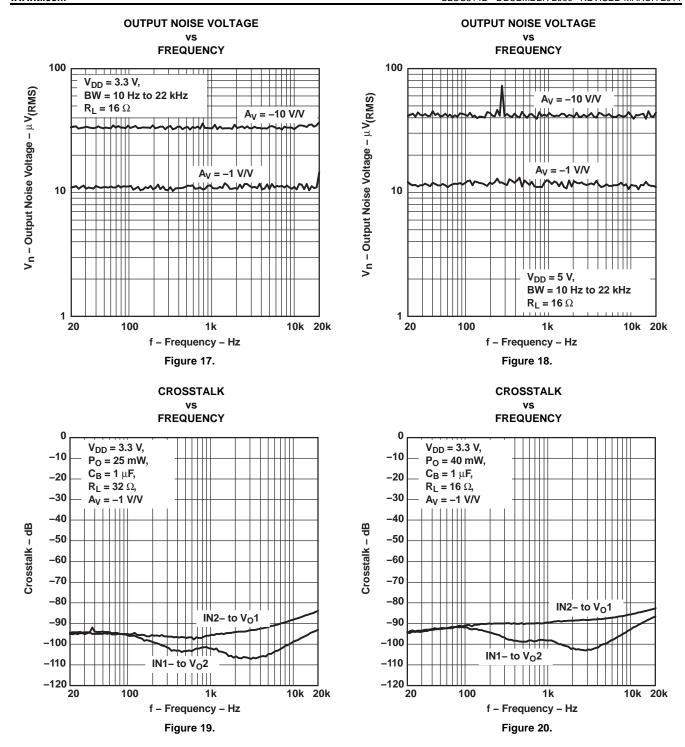
#### **SUPPLY RIPPLE REJECTION RATIO**

Figure 14.

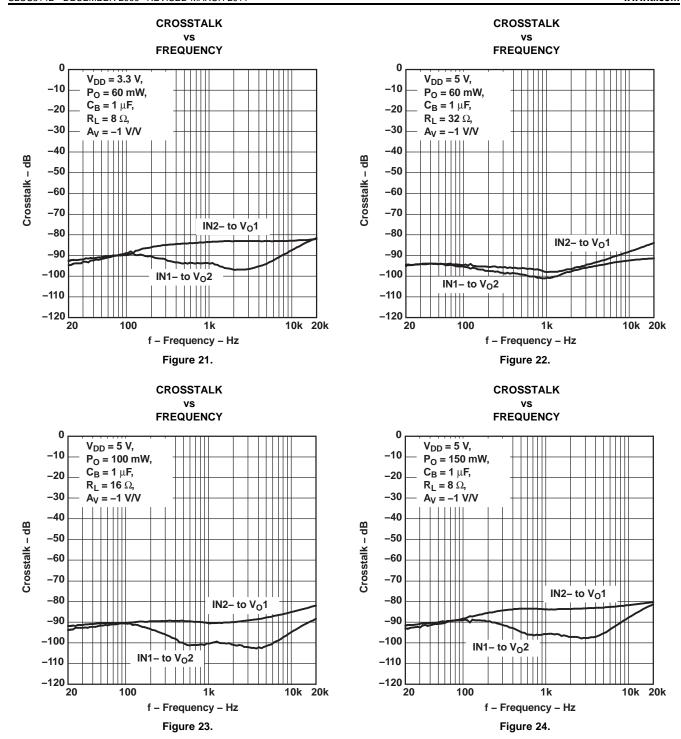
#### VS











SHUTDOWN ATTENUATION



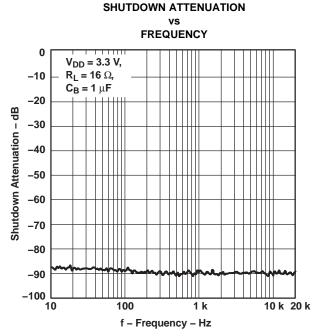


Figure 25.

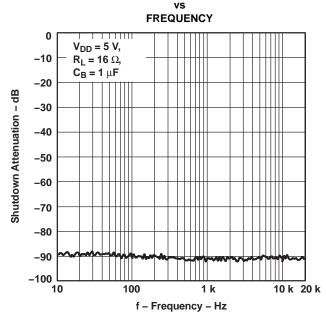
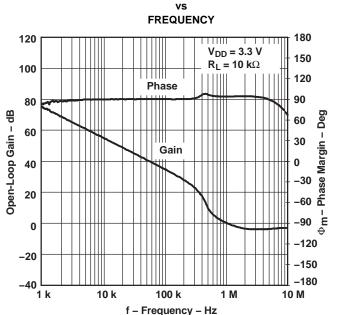


Figure 26.

### **OPEN-LOOP GAIN AND PHASE MARGIN**



OPEN-LOOP GAIN AND PHASE MARGIN

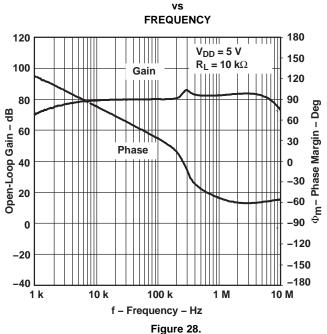
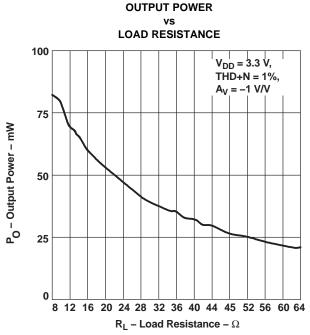
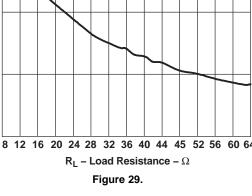
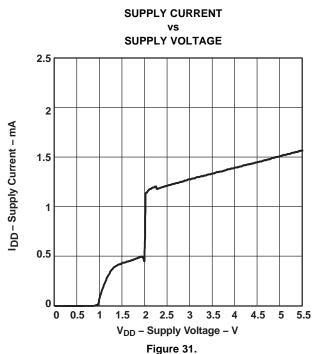


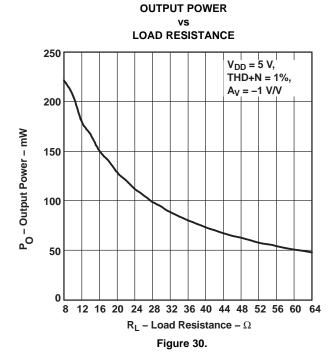
Figure 27.

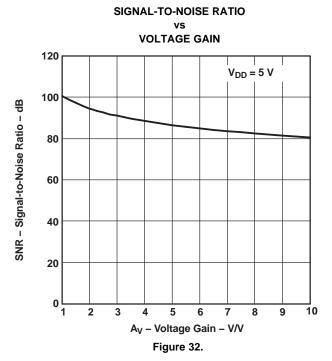






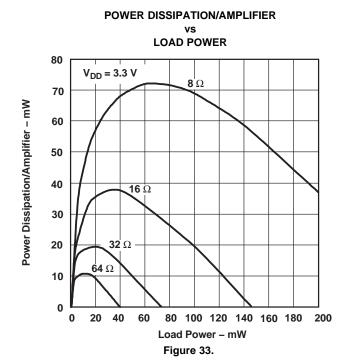


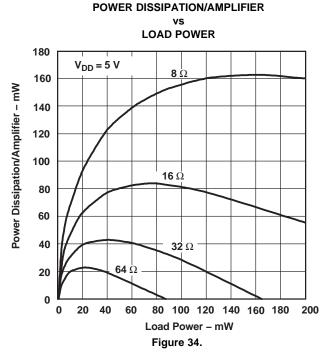




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#### APPLICATION INFORMATION

#### GAIN SETTING RESISTORS, R<sub>f</sub> and R<sub>i</sub>

The gain for the TPA6110A2 is set by resistors  $R_f$  and  $R_i$  according to Equation 1.

$$Gain = -\left(\frac{R_f}{R_i}\right)$$
 (1)

Given that the TPA6110A2 is a MOS amplifier, the input impedance is very high. Consequently input leakage currents are not generally a concern. However, noise in the circuit increases as the value of  $R_{\rm f}$  increases. In addition, a certain range of  $R_{\rm f}$  values is required for proper start-up operation of the amplifier. Considering these factors, it is recommended that the effective impedance seen by the inverting node of the amplifier be set between 5  $k\Omega$  and 20  $k\Omega$ . The effective impedance is calculated using Equation 2.

Effective Impedance = 
$$\frac{R_f R_i}{R_f + R_i}$$
 (2)

For example, if the input resistance is 20  $k\Omega$  and the feedback resistor is 20  $k\Omega,$  the gain of the amplifier is -1, and the effective impedance at the inverting terminal is 10  $k\Omega,$  a value within the recommended range.

For high performance applications, metal-film resistors are recommended because they tend to have lower noise levels than carbon resistors. For values of  $R_{\rm f}$  above 50 k $\Omega$ , the amplifier tends to become unstable due to a pole formed from  $R_{\rm f}$  and the inherent input capacitance of the MOS input structure. For this reason, a small compensation capacitor of approximately 5 pF should be placed in parallel with  $R_{\rm f}$ . This, in effect, creates a low-pass filter network with the cutoff frequency defined by Equation 3.

$$f_{c(lowpass)} = \frac{1}{2\pi R_f C_F}$$
 (3)

For example, if  $R_f$  is 100  $k\Omega$  and  $C_F$  is 5 pF then  $f_{c(lowpass)}$  is 318 kHz, which is well outside the audio range.

#### INPUT CAPACITOR, Ci

In the typical application, an input capacitor,  $C_i$ , is required to allow the amplifier to bias the input signal to the proper dc level for optimum operation. In this case,  $C_i$  and  $R_i$  form a high-pass filter with the corner frequency determined in Equation 4.

$$f_{c(highpass)} = \frac{1}{2\pi R_i C_i}$$
 (4)

The value of  $C_i$  directly affects the bass (low frequency) performance of the circuit. Consider the example where  $R_i$  is 20 k $\Omega$  and the specification calls for a flat bass response down to 20 Hz. Equation 4 is reconfigured as Equation 5.

$$C_{i} = \frac{1}{2\pi R_{i} f_{c(highpass)}}$$
 (5)

In this example,  $C_i$  is 0.40  $\mu F$ , so one would likely choose a value in the range of 0.47  $\mu F$  to 1  $\mu F$ . A further consideration for this capacitor is the leakage path from the input source through the input network formed by  $R_i$ ,  $C_i$ , and the feedback resistor ( $R_f$ ) to the load. This leakage current creates a dc offset voltage at the input to the amplifier that reduces useful headroom, especially in high-gain applications (gain >10). For this reason a low-leakage tantalum or ceramic capacitor is the best choice. When polarized capacitors are used, connect the positive side of the capacitor to the amplifier input in most applications. The dc level there is held at  $V_{DD}/2$ —likely higher than the source dc level. It is important to confirm the capacitor polarity in the application.

### POWER SUPPLY DECOUPLING, C(S)

The TPA6110A2 is a high-performance CMOS audio amplifier that requires adequate power-supply decoupling to minimize the output total harmonic distortion (THD). Power-supply decoupling also prevents oscillations when long lead lengths are used between the amplifier and the speaker. The optimum decoupling is achieved by using two capacitors of different types that target different types of noise on the power supply leads. For higher frequency transients, spikes, or digital hash on the line, a good equivalent-series-resistance (ESR) capacitor, typically 0.1 µF, placed as close as possible to the device V<sub>DD</sub> lead, works best. For filtering lower-frequency noise signals, a larger aluminum electrolytic capacitor of 10 µF or greater placed near the power amplifier is recommended.

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### MIDRAIL BYPASS CAPACITOR, C(B)

The midrail bypass capacitor,  $C_{(B)}$ , serves several important functions. During start up,  $C_{(B)}$  determines the rate at which the amplifier starts up. This helps to push the start-up pop noise into the subaudible range (so low it can not be heard). The second function is to reduce noise produced by the power supply caused by coupling into the output drive signal. This noise is from the midrail generation circuit internal to the amplifier. The capacitor is fed from a 230-k $\Omega$  source inside the amplifier. To keep the start-up pop as low as possible, maintain the relationship shown in Equation 6.

$$\frac{1}{\left(C_{(B)} \times 230 \text{ k}\Omega\right)} \leq \frac{1}{\left(C_{i}R_{i}\right)} \tag{6}$$

Consider an example circuit where  $C_{(B)}$  is 1  $\mu$ F,  $C_i$  is 1  $\mu$ F, and  $R_i$  is 20  $k\Omega$ . Substituting these values into the equation 9 results in:  $6.25 \le 50$  which satisfies the rule. Bypass capacitor,  $C_{(B)}$ , values of 0.1  $\mu$ F to 1  $\mu$ F ceramic or tantalum low-ESR capacitors are recommended for the best THD and noise performance.

### OUTPUT COUPLING CAPACITOR, C(C)

In a typical single-supply, single-ended (SE) configuration, an output coupling capacitor  $(C_{(C)})$  is required to block the dc bias at the output of the amplifier, thus preventing dc currents in the load. As with the input coupling capacitor, the output coupling capacitor and impedance of the load form a high-pass filter governed by Equation 7.

$$f_{C} = \frac{1}{2\pi R_{L} C_{(C)}} \tag{7}$$

The main disadvantage, from a performance standpoint, is that the typically-small load impedance drives the low-frequency corner higher. Large values of  $C_{(C)}$  are required to pass low frequencies into the load. Consider the example where a  $C_{(C)}$  of 68  $\mu F$  is chosen and loads vary from 32  $\Omega$  to 47 k $\Omega$ . Table 1 summarizes the frequency response characteristics of each configuration.

Table 1. Common Load Impedances vs Low-Frequency Output Characteristics in SE Mode

R <sub>L</sub>	C <sub>(C)</sub>	LOWEST FREQUENCY
32 Ω	68 µF	73 Hz
10,000 Ω	68 µF	0.23 Hz
47,000 Ω	68 µF	0.05 Hz

As Table 1 indicates, headphone response is adequate, and drive into line level inputs (a home stereo for example) is very good.

The output coupling capacitor required in single-supply SE mode also places additional constraints on the selection of other components in the amplifier circuit. With the rules described earlier still valid, add the following relationship:

$$\frac{1}{\left(C_{(B)} \times 230 \text{ k}\Omega\right)} \leq \frac{1}{\left(C_{i}R_{i}\right)} \ll \frac{1}{R_{L}C_{(C)}}$$
(8)

#### **USING LOW-ESR CAPACITORS**

Low-ESR capacitors are recommended throughout this application. A real capacitor can be modeled simply as a resistor in series with an ideal capacitor. The voltage drop across this resistor minimizes the beneficial effects of the capacitor in the circuit. The lower the equivalent value of this resistance, the more the real capacitor behaves like an ideal capacitor.

#### **5-V VERSUS 3.3-V OPERATION**

The TPA6110A2 was designed for operation over a supply range of 2.5 V to 5.5 V. This data sheet provides full specifications for 5-V and 3.3-V operation, since these are considered to be the two most common supply voltages. There are no special considerations for 3.3-V versus 5-V operation as far as supply bypassing, gain setting, or stability. The most important consideration is that of output power. Each amplifier in theTPA6110A2 can produce a maximum voltage swing of  $V_{DD}-1$  V. This means, for 3.3-V operation, clipping starts to occur when  $V_{O(PP)}=2.3$  V as opposed when  $V_{O(PP)}=4$  V while operating at 5 V. The reduced voltage swing subsequently reduces maximum output power into the load before distortion becomes significant.



### **REVISION HISTORY**

CI	nanges from Original (December 2000) to Revision A	Page
•	Change the DC ELECTRICAL CHARACTERISTICS table From $T_A$ = 25°C, $V_{DD}$ = 3.3 V To: $T_A$ = 25°C, $V_{DD}$ = 2.5 V, updated values	
•	Change the DC ELECTRICAL CHARACTERISTICS table From $T_A = 25^{\circ}C$ , $V_{DD} = 5$ V To: $T_A = 25^{\circ}C$ , $V_{DD} = 5.5$ V, updated values	3
•	Changed Figure 8, From: $R_L = 8k\Omega$ To: $R_L = 8\Omega$	<u>6</u>
•	Changed Figure 24, From: frequency limit at 1M To: frequency limit at 20K	10
<u>.</u>	Changed Figure 25, From: frequency limit at 1M To: frequency limit at 20K	11
CI	nanges from Revision A (September 2004) to Revision B	Page
	Changed the DC Electrical Characteristice ( $V_{DD} = 2.5V$ ) for $I_{DD(SD)}$ From: Typ = 10 Max = 50 To: Typ = 1 Max = 10 .	3
•	Changed the DC Electrical Characteristice ( $V_{DD} = 5.5V$ ) for $I_{DD(SD)}$ From: Typ = 60 Max = 100 To: Typ = 1 Max = 10	3

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#### PACKAGING INFORMATION

Orderable Device	Status	Package Type	Package Drawing	Pins	Package Qty	Eco Plan	Lead finish/ Ball material	MSL Peak Temp	Op Temp (°C)	Device Marking (4/5)	Samples
							(6)				
TPA6110A2DGN	ACTIVE	HVSSOP	DGN	8	80	RoHS & Green	NIPDAU   NIPDAUAG	Level-1-260C-UNLIM	-40 to 85	AIZ	Samples
TPA6110A2DGNG4	ACTIVE	HVSSOP	DGN	8	80	RoHS & Green	NIPDAU	Level-1-260C-UNLIM	-40 to 85	AIZ	Samples
TPA6110A2DGNR	ACTIVE	HVSSOP	DGN	8	2500	RoHS & Green	NIPDAU   NIPDAUAG	Level-1-260C-UNLIM	-40 to 85	AIZ	Samples

(1) The marketing status values are defined as follows:

**ACTIVE:** Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

**OBSOLETE:** TI has discontinued the production of the device.

(2) RoHS: TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".

RoHS Exempt: TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.

Green: TI defines "Green" to mean the content of Chlorine (CI) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the <=1000ppm threshold requirement.

- (3) MSL, Peak Temp. The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.
- (4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.
- (5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.
- (6) Lead finish/Ball material Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

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# **PACKAGE OPTION ADDENDUM**

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In no event shall TI's liability arising out of such information exceed the total purchase price of the TI part(s) at issue in this document sold by TI to Customer on an annual basis.

## PACKAGE MATERIALS INFORMATION

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### TAPE AND REEL INFORMATION





	Dimension designed to accommodate the component width
B0	Dimension designed to accommodate the component length
K0	Dimension designed to accommodate the component thickness
W	Overall width of the carrier tape
P1	Pitch between successive cavity centers

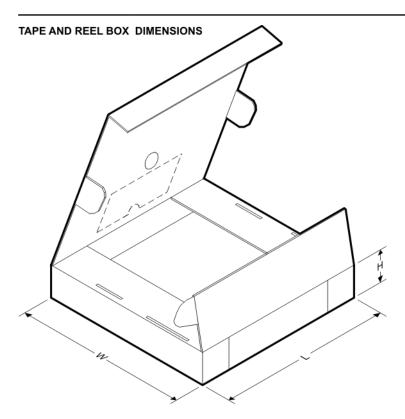
QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE



#### \*All dimensions are nominal

I	Device	Package Type	Package Drawing		SPQ	Reel Diameter	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
	TPA6110A2DGNR	HVSSOP	DGN	8	2500	(mm) 330.0	12.4	5.3	3.4	1.4	8.0	12.0	Q1
	TPA6110A2DGNR	HVSSOP	DGN	8	2500	330.0	12.4	5.3	3.4	1.4	8.0	12.0	Q1

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#### \*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
TPA6110A2DGNR	HVSSOP	DGN	8	2500	358.0	335.0	35.0
TPA6110A2DGNR	HVSSOP	DGN	8	2500	364.0	364.0	27.0

## PACKAGE MATERIALS INFORMATION

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#### **TUBE**



#### \*All dimensions are nominal

Device	Package Name	Package Type	Pins	SPQ	L (mm)	W (mm)	T (µm)	B (mm)
TPA6110A2DGN	DGN	HVSSOP	8	80	330	6.55	500	2.88
TPA6110A2DGNG4	DGN	HVSSOP	8	80	330	6.55	500	2.88

3 x 3, 0.65 mm pitch

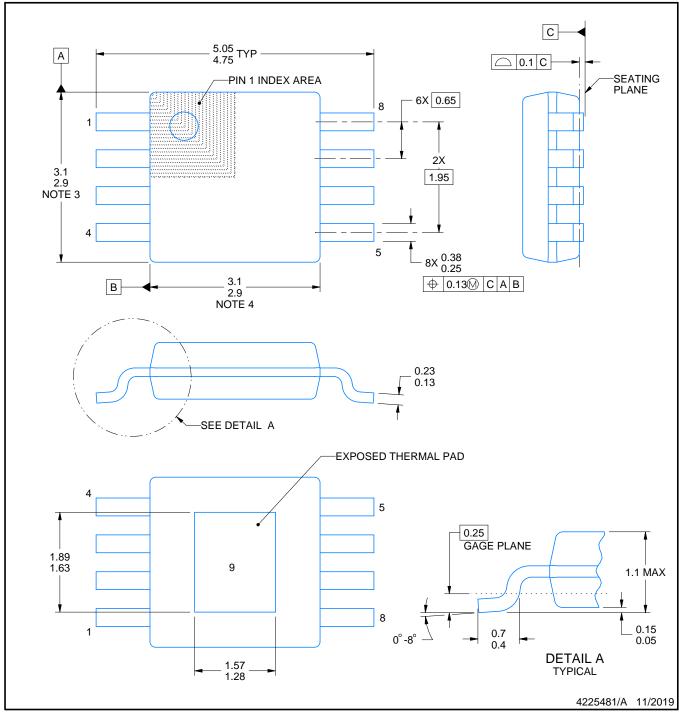
SMALL OUTLINE PACKAGE

This image is a representation of the package family, actual package may vary. Refer to the product data sheet for package details.



# $\textbf{PowerPAD}^{^{\text{\tiny{TM}}}}\,\textbf{VSSOP - 1.1 mm max height}$

SMALL OUTLINE PACKAGE



#### NOTES:

PowerPAD is a trademark of Texas Instruments.

- 1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.

  2. This drawing is subject to change without notice.

  3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not
- exceed 0.15 mm per side.
- 4. This dimension does not include interlead flash. Interlead flash shall not exceed 0.25 mm per side.
- 5. Reference JEDEC registration MO-187.



SMALL OUTLINE PACKAGE



#### NOTES: (continued)

- 6. Publication IPC-7351 may have alternate designs.
- 7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.
- 8. Vias are optional depending on application, refer to device data sheet. If any vias are implemented, refer to their locations shown on this view. It is recommended that vias under paste be filled, plugged or tented.
- 9. Size of metal pad may vary due to creepage requirement.



SMALL OUTLINE PACKAGE



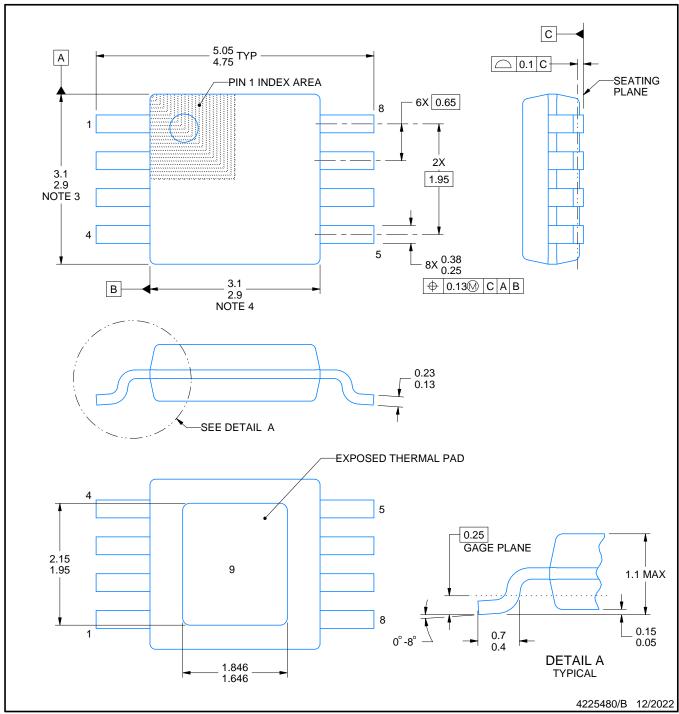
NOTES: (continued)

- 10. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
- 11. Board assembly site may have different recommendations for stencil design.



# $\textbf{PowerPAD}^{^{\text{\tiny{TM}}}}\,\textbf{VSSOP - 1.1 mm max height}$

SMALL OUTLINE PACKAGE



#### NOTES:

PowerPAD is a trademark of Texas Instruments.

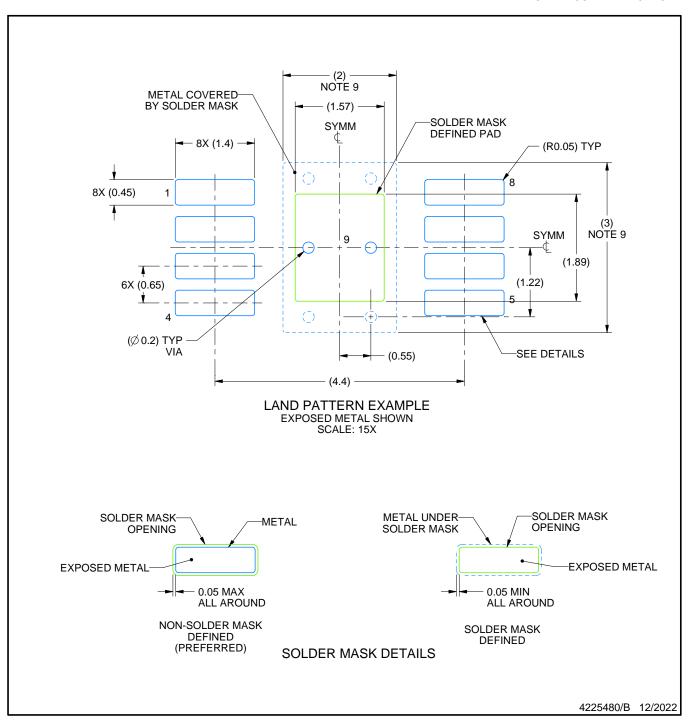
- 1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.

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SMALL OUTLINE PACKAGE

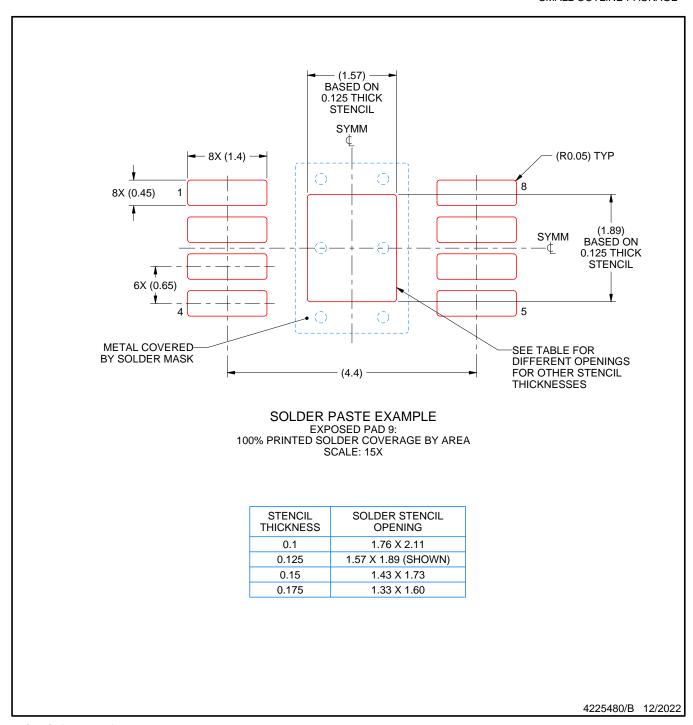


#### NOTES: (continued)

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- 7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.
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SMALL OUTLINE PACKAGE



NOTES: (continued)

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- 11. Board assembly site may have different recommendations for stencil design.



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